A FINITE DIFFERENCE METHOD FOR THE EXCITATION OF A DIGITAL WAVEGUIDE STRING MODEL

Leonardo Gabrielli¹, Luca Remaggi¹, Stefano Squartini¹ and Vesa Välimäki²

 1 Universitá Politecnica delle Marche, Ancona, Italy 2 Aalto University, Espoo, Finland

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Aalto University



Who's Who



3MediaLabs: Multimedia Information Processing

Made of two research sub-groups: *A3LAB* and *SEMEDIA*. LEADER: Prof. Francesco Piazza

A3LAB: DSP Algorithms and Adaptive systems for Audio applications

- Data Processing Approach
- People: 2 Assistant Professors, 4 PostDocs, 4 Phd Students

SEMEDIA: Semantic Web and Multimedia

- MetaData Processing Approach
- People: 3 PostDocs





Wave Equation Solutions



Ideal String Wave Equation

$$\frac{\partial^2 y}{\partial t^2} = c^2 \frac{\partial^2 y}{\partial x^2}$$
(1)
(d'Alembert, 1747)



1D DWG

General solution found by d'Alembert in 1747:

$$y(k, n+1) = gy^{+}(k-1, n) + gy^{-}(k+1, n)$$
(2)



Consolidating the delays and gains yields extremely computational efficient solutions $% \left({{{\left[{{{\left[{{\left[{{\left[{{\left[{{\left[{{{\left[{{{\left[{{{\left[{{\left[{{{\left[{{{\left[{{{\left[{{{\left[{{{}}}} \right]}}}} \right.$



First Order FDTD Scheme (FOFS)

Central differences scheme:

$$y_{k,n+1} = g_k^+ y_{k-1,n} + g_k^- y_{k+1,n} + a_k y_{k,n-1}$$
(3)

$$g_{k+1}^{*} \qquad g_{k+1}^{*} \qquad g_{k+1}^{*} \qquad g_{k+1}^{*} \qquad g_{k+1,n+1}^{*} \qquad g_{k+1,n+1}$$



Stiff strings are also characterized by dispersion, the new wave equation is:

$$\frac{\partial^2 y}{\partial t^2} = c \frac{\partial^2 y}{\partial x^2} - \lambda \frac{\partial^4 y}{\partial x^4} - 2\sigma_0 \frac{\partial y}{\partial t} + 2\sigma_1 \frac{\partial y}{\partial t} \frac{\partial^2 y}{\partial x^2}$$
(4)

- λ stiffness,
- σ_0 f-independent loss
- σ_1 f-dependent loss



Second order FDTD scheme (SOFS)

A numerical scheme for the PDE (4) after [Bilbao, 2010]

$$y_{k,n+1} = a_0 y_{k,n} + a_1 (y_{k+1,n} + y_{k-1,n}) + + a_2 (y_{k+2,n} + y_{k-2,n}) + b_0 y_{k,n-1} + + b_1 (y_{k+1,n-1} + y_{k-1,n-1})$$
(5)





FOFS vs. SOFS	
n+1 ●	n+1 ●
n O O	n O O O O O
n-1 O	n-1 O O O
k-1 k k+1	k-2 k-1 k k+1 k+2
FOFS for (1)	SOFS for (4)



Pros and Cons

DWG

- Efficiency
- Numerical stability
- Flexible addition of DSP blocks

- Departure from underlying physics
- Characterization based on audio analysis

FDTD

- Characterization based on physical measurement
- Minimal precomputation of parameters
- Emulation of distributed nonlinear contact

- Computational cost (not an issue anymore)
- Coefficients design



Interfacing DWG and FDTD



Previous works

Mixed modeling

- M. Karjalainen, C. Erkut, and L. Savioja, "Compilation of unified physical models for efficient sound synthesis", in Acoustics, Speech, and Signal Processing, 2003. Proceedings.(ICASSP 03) 2003 IEEE International Conference on. IEEE, 2003, vol. 5, pp. V-433.
- M. Karjalainen and C. Erkut, "Digital Waveguides versus Finite Difference Structures: Equivalence and Mixed Modeling", EURASIP Journal on Advances in Signal Processing, no. 7, pp. 978-989, 2004.





Mixed Modeling Goals

- Unified approach (1 POV)
- Modular modeling (many
- FDTD features at a lower cost



SOFS-DWG Interface Conditions for Matching

$$\begin{split} y_{k,n+1} &= a_0 y_{k,n} + \\ &+ a_1 (y_{k-1,n} + y_{k+1,n}) + \\ &+ b_1 (y_{k-1,n-1} + y_{k+1,n-1}) + \\ &+ b_0 y_{k,n-1} + a_2 (y_{k-2,n} + y_{k+2,n}) \quad \ \ (6) \\ \text{with k: last FDTD spatial point} \end{split}$$

$$y_{k+1,n}^{+} = y_{k+1,n-1}^{-} + gy_{k,n}$$
 (7)

with k+1: first DWG spatial point





Case Study



Hohner Clavinet D6





Mechanical Action



Polynomial Pulse Model (PPM)

$$f(x) = a_p x^p + a_{p-1} x^{p-1} + \dots + a_1 x + a_0$$
(8)



Spectral Envelope Model (SEM)

$$E = \alpha_1 E_1 + (1 - \alpha) E_2$$
 (9)



Proposed Excitation Model I	
Tangent force: • $f_{tan} = \theta(k) f_{max} \phi(t)$ (derived from [Bilbao, 2010])	• $\phi(t)$: raised cosine (1-4 ms) • f_{max} : maximum force (10 N) • $\theta(k)$: localization
Contact length [smp]: • $e = l_c/h$	l_c : tangent width h: grid spacing
Localization	
$if: 0 < e \le 2$ Concentrated contact w/ linear interpolation $\theta(k) = \begin{cases} \frac{1}{e}, & k = k_i \\ \frac{b}{e}, & k = k_{i+1} \\ 0, & \text{otherwise} \end{cases} (10)$	Distributed contact w/ Lagrange interpolation (f-resp: -6 dB at Nyquist) $\theta(k) = \begin{cases} \frac{(e-1)(e-2)}{2}, & k = k_{i-1} \\ -e(e-2), & k = k_i \\ \frac{e(e-1)}{2}, & k = k_{i+1} \\ 0, & \text{otherwise} \end{cases}$ (11)

Proposed Excitation Model II	
Stud force • $f_{stud} = K(y_k)^{\alpha} \theta(x)$	 <i>K</i>: stiffness coefficient <i>α</i> : penetration coefficient



Resume

- Tangent contact: FDTD
- Wave propagation: DWG
- $\bullet\,$ Secondary effects (e.g. beating, pickups): additional filters cascaded to the DWG

 $\mathsf{FDTD} \leftrightarrow \mathsf{DWG} \longrightarrow \mathsf{Secondary} \; \mathsf{EFX}$



Simulations



Video: Computer Simulation



Computational Cost



Notes:

- DWG has a constant overhead due to constant filters order
- $\bullet~50\%$ string in FDTD and 50% in DWG

samples at http://a3lab.dii.univpm.it/projects/fdtd-adaptor



Conclusions



Outcome

- A novel SOFS-DWG adaptor is devised to extend previous FOFS-DWG modeling
- Reduced Computational Cost compared to FDTD
- Increased flexibility: excitation-related parameters are physical...
- ...but missing perceptual components can be added with standard DWG methods

Future Work

- Listening Tests similarly to [Gabrielli, 2011]
- Evaluate the mixed approach ease of parametrization



Thank you



References



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